Transformer tank vibration modeling as a method of detecting winding deformations — Part I: Theoretical foundation (2006)

Paper

Follow-up verification paper

Abstract

> In this paper, a model developed for a transformer monitoring system to estimate transformer tank vibration is presented. The model calculates vibration on the transformer tank starting from some input variables that can be easily measured on the transformer. Tank vibration is also measured, showing a good concordance between estimated and measured values if the transformer is healthy. In case of a winding deformation winding vibration and, consequently, that of the tank, changes and a big difference between estimated and measured vibration appear. To estimate tank vibration, the model takes into account the main physical phenomena generating vibrations in the different transformer elements and how these vibrations are superposed and transmitted to the tank. The model has been tested experimentally on a test transformer fitted with internal and external accelerometers. A deformation has been provoked in the test transformer winding with the aim of testing the

> model’s ability to detect it. The model has been also tested on several in-service grid transformers. The results of the experimental validation are shown in Part II of the paper.

Introduction

- 12-15% of transformer failures are caused by winding deformations
  - provoked by high electrodynamic forces caused during a short-circuit event
    - I wonder if GridScan can detect this
  - this paper is old, Cigré says it's 45% now

Vibration Model

- winding vibrations
  - electrodynamic forces caused by the interaction of the current in the winding with leakage flux
- core vibrations
  - magnetostriction
  - magnetic forces
- magnetostriction is proportional to voltage squared
  - dependent upon temperature
- load tap changer (LTC) vibrations might be >1 kHz

Transformer Vibrations

- on page 3 it says "the winding and the core vibration are proportional to the current and voltage squared, respectively"
  - phase angle between them correlates to the power facto
  - how do I separate these two?

Vibrational Experimental Analysis

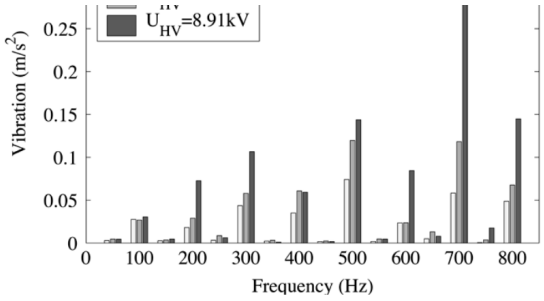


Fig. 5. Central phase winding vibration in an axial direction (accelerometer ac5) for different applied voltages with the transformer on no load.

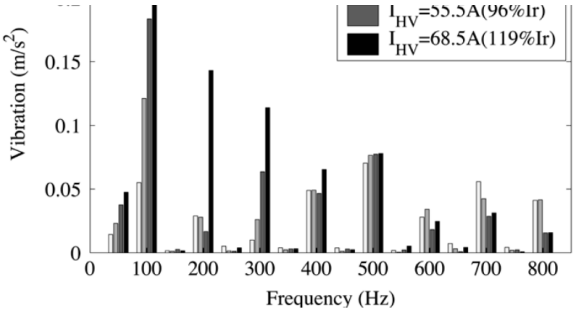


Fig. 6. Winding axial vibrations (accelerometer ac5) for different loads.

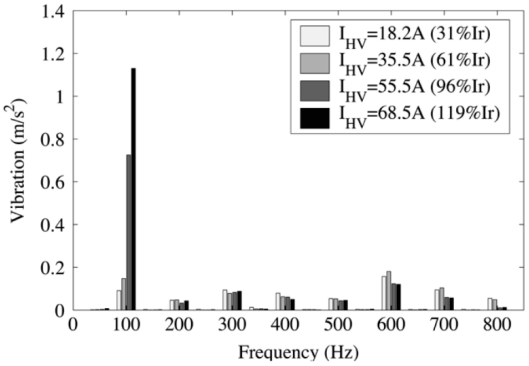


Fig. 8. Vibrations of the bottom part of the tank (accelerometer ac14) for different loads.

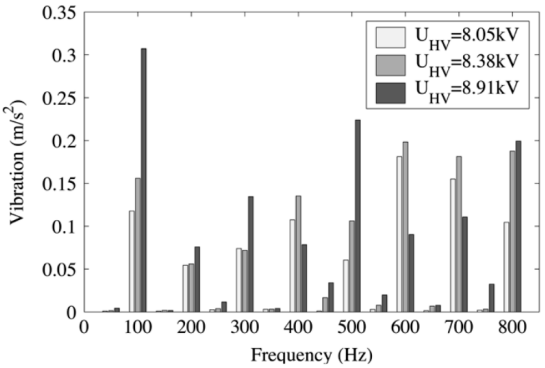


Fig. 10. No-load vibrations at the bottom of the tank (accelerometer ac14).

Power Factor

- the imaginary part of frequency amplitude barely changed when a pump (pf 0.7) was turned on
  - 100 Hz increased slightly
  - maybe it correlates with the reactive loading?

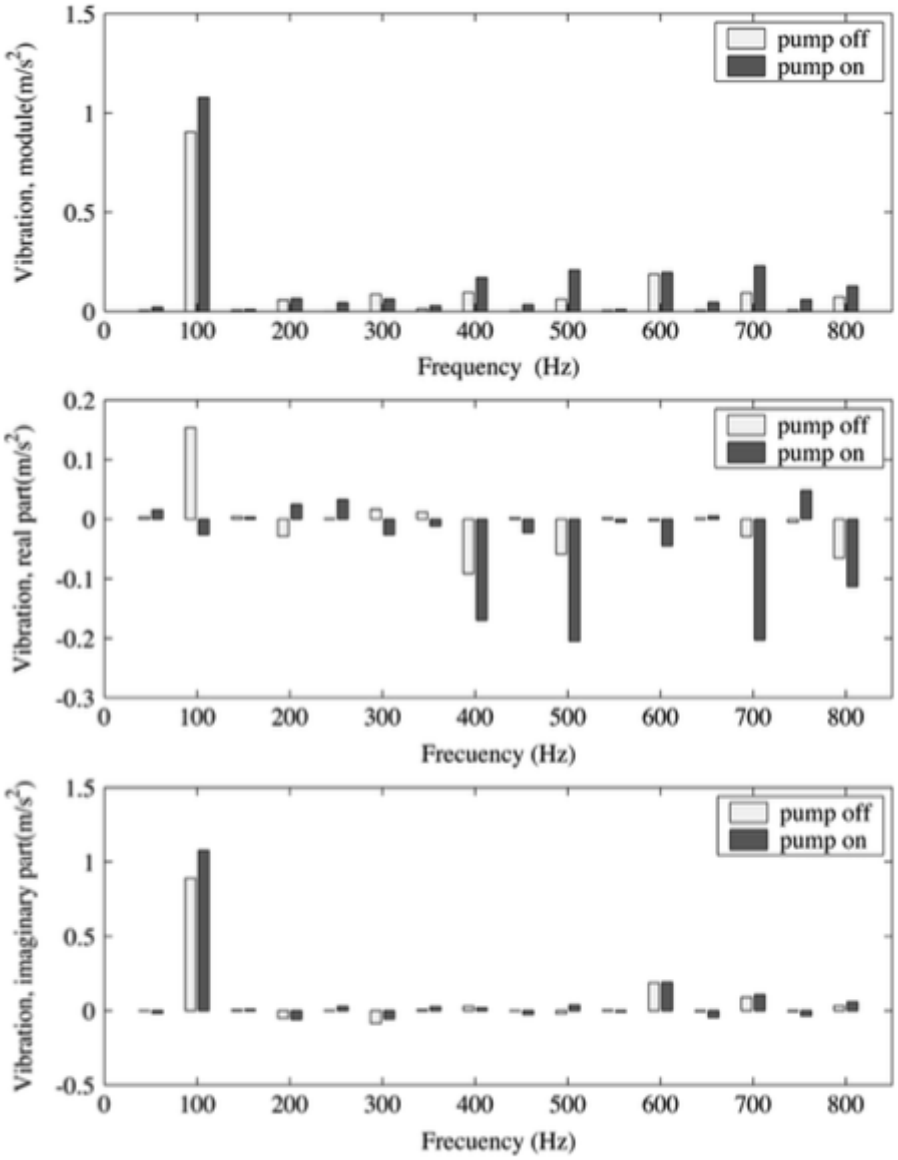


Fig. 12. Vibration in the bottom of the tank (accelerometer ac14) for natural oil circulation and forced oil circulation.

Conclusion

- no real way to discern core noise from winding noise
  - > can't find where it says that in the paper
  - especially because on page 3 it says "the winding and the core vibration are proportional to the current and voltage squared, respectively"
  - phase angle between them correlates to the power factor
- overloading is going to be BAD for 2nd and 3rd harmonics
  - why? I thought rated loading was an artificial limit vs physical
    - appears not!
- 50 Hz is proportional to loading
  - I'm still pretty sure this is just the shaking of the transformer due to pixies dancing in unison

    - update: the 50 Hz is due to DC bias/phase imbalance
- winding vibration is linear with square of current
    - 1st, 2nd, 3rd
- voltage
    - 2nd, 3rd, 5th, 7th, 8th (fig 5)
        - maybe 4th, 6th
        - might as well just list everything
    - measured on windings
- current
    - 1st (fig 8)
    - 0.5th, 1st, 2nd (?), 3rd (fig 6)

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